

# Description and parameterization of turbulence in the marine atmospheric boundary layer VERITAS TUFFO

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Coordination

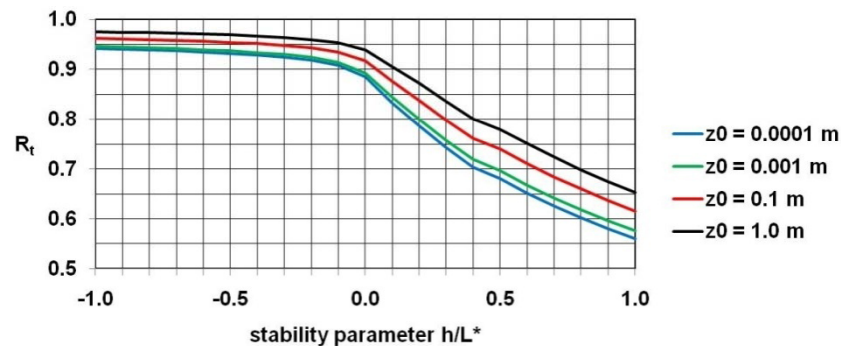
## **Meteorological challenges for offshore wind parks:**

- **marine atmospheric boundary layer is different:**
  - **shallow atmospheric boundary layer**
  - **wind speed-dependent roughness and turbulence**
  - **wind direction and season-dependent atmospheric stability and turbulence**
  - **stability-independent vertical gradient of atmospheric humidity**
- **necessity for reliable wind field models with correct description/parameterization of turbulence**

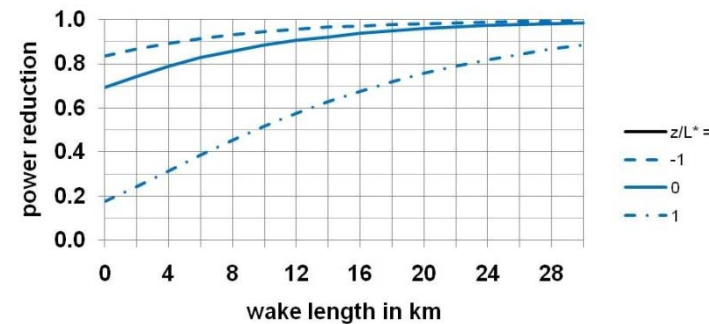
## Turbulence

- influences loads on wind turbines (negative)
- influences harvests from wind turbines (positive)
- influences wind park efficiency (positive)
- influences wake lengths behind turbines and wind parks (positive)

power yield from large wind parks



available power behind large wind parks



← more turbulence less turbulence →

Emeis, S., 2010: A simple analytical wind park model considering atmospheric stability. Wind Energy, 13, 459-469.



## VERITAS results

## VERITAS (July 1, 2008 to December 31, 2011)

**V**erification of **t**urbulence parameterization and description of the vertical structure of the maritime **a**tmospheric boundary layer in numerical **s**imulation models for wind analysis and forecast

became work package 5 of OWEA (see sessions 3 and 5 this morning)

**investigators:**

**Richard Foreman M. Sc. (his PhD work, successfully completed Nov 31, 2011)**  
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## drag coefficient (neutral thermal stratification)

usual approach:

$$C_{Dn} = u_*^2 / U^2 \quad (\text{friction velocity over 10 m wind speed})$$

$$= \kappa^2 / \ln^2(z/z_0) \quad (\text{over land: logarithmic profile})$$



$C_{Dn}$  is function of surface properties only

$$= \kappa^2 / \ln^2(gz/\alpha u_*^2) \quad (\text{over sea: Charnock's relation})$$



$C_{Dn}$  depends on wind speed as well

empirically:

$$C_{D10n} = 0.000063 U_{10} + 0.00061 \quad (\text{Smith 1980})$$

**no wave data available:**

**within the fully turbulent regime:**

**friction velocity:**

$$u_* = 0.051 U_{10} - 0.14$$

**input to the definition of  $C_D$ :**

$$C_{D10n} = (0.051 U_{10} - 0.14)^2 / U_{10}^2$$

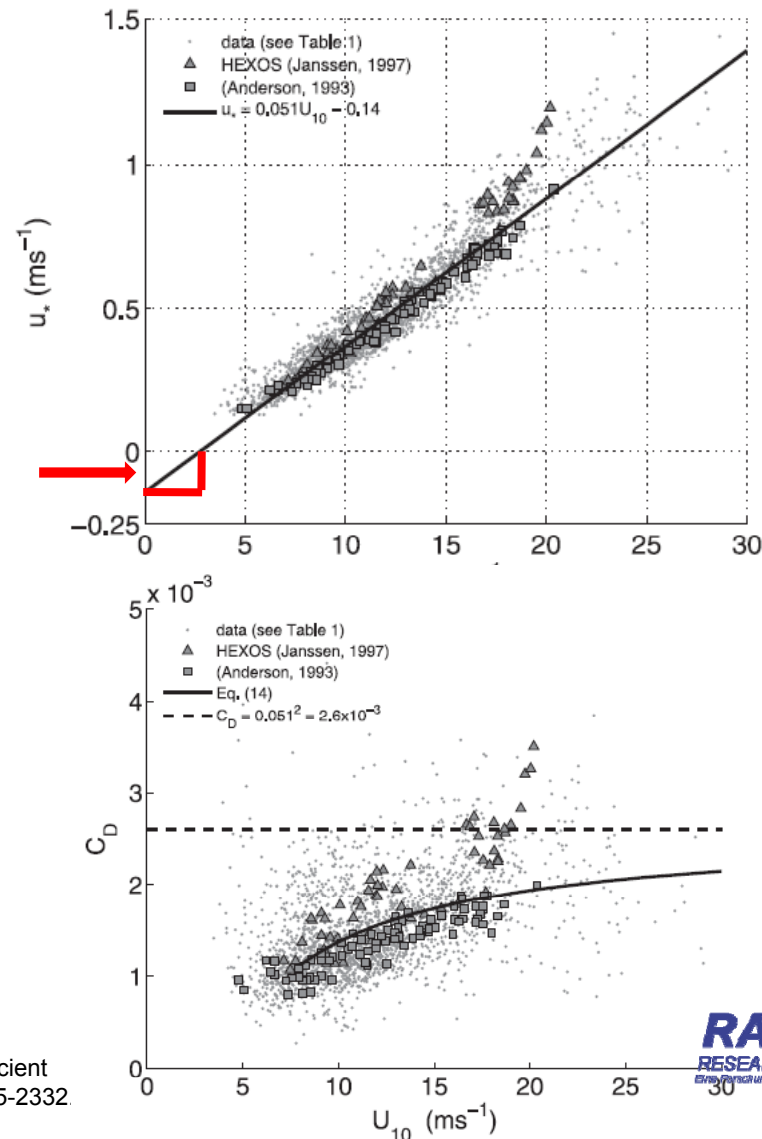
$$C_{D10n} = (C_m U_{10} - b)^2 / U_{10}^2$$

**approaches:**

$$C_m^2 = 0.051^2 = 0.0026$$

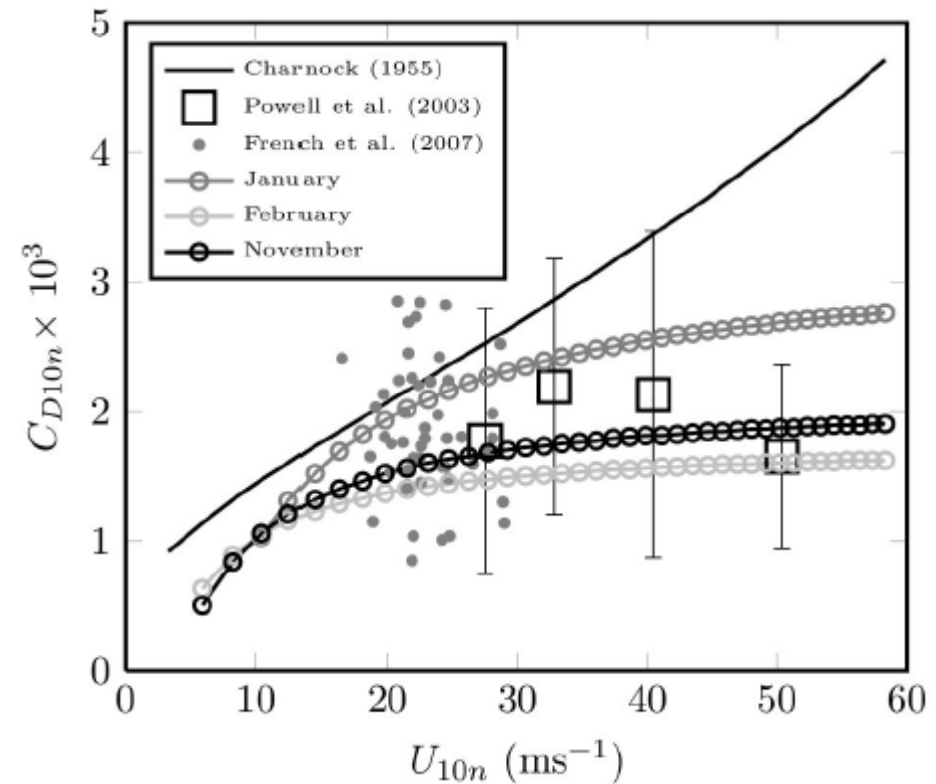
**for large  $U_{10}$**

Foreman, R., S. Emeis, 2010: Revisiting the Definition of the Drag Coefficient in the Marine Atmospheric Boundary Layer. J. Phys. Oceanogr., **40**, 2325-2332.



## Comparison with data:

	$C_m$	b
Literatur	0.051	0.14 m/s
FINO Jan 2005	0.057	0.26 m/s
FINO Feb 2005	0.042	0.01 m/s
FINO Nov 2005	0.048	0.02 m/s



🔍  $C_{D10n}$  still depends on wind speed (but at least:  $C_m$  does not)  
the plot shows a non-dimensional variable plotted against a dimensional one



## wave data available:

$$C_{D10n} = a (H_s/\lambda_p)^2 \quad (\text{from dimensional analysis})$$

the drag coefficient should not approach zero for vanishing waves. Therefore a minimum is set:

$$C_{D10n} = 0.0009 \quad (\text{smooth surface})$$

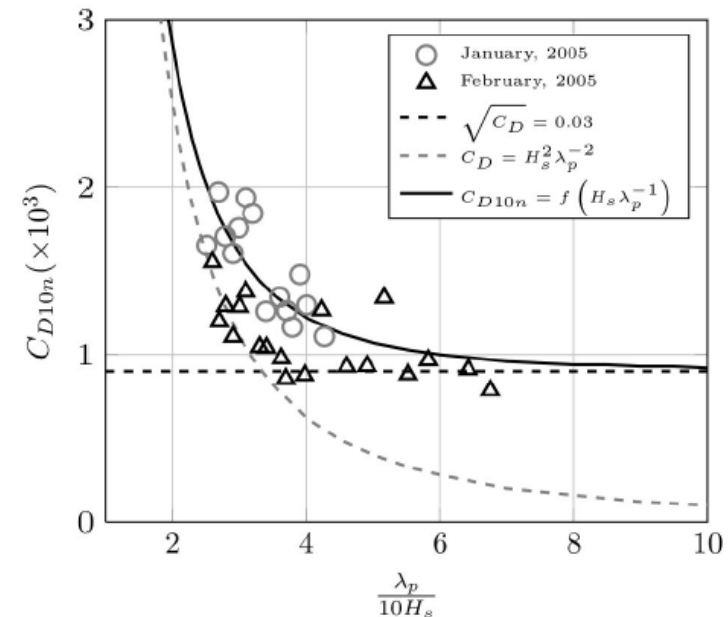
fit between both extremes:

$$(C_{D10n}^{1/2})^n = 0.03^n + (H_s/\lambda_p)^n$$

empirically  $n \approx 3$

(Churchill and Usagi 1972)

- ☺  $C_{D10n}$  depends on surface parameter only
- ☺ both axes in plot are now non-dimensional



steep ←

→ shallow

**turbulence parameterization in meso-scale wind field models  
such as MM5 or WRF:**

	A1	A2	B1	B2	C1
MY 1982	0.92	0.74	16.6	10.1	0.08
MYJ 2002	0.660	0.657	11.878	7.227	0.00083
<b>new</b>	<b>0.91</b>	<b>0.54</b>	<b>28.76</b>	<b>13.08</b>	<b>0.15</b>

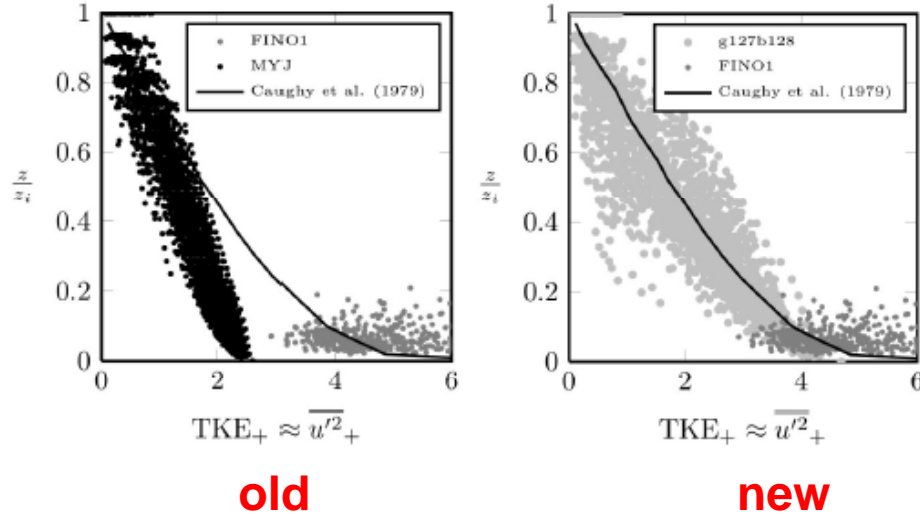
**plus an adaptation of turbulent length scales following Nakanishi (2001)**

**new values are based on modern laboratory data**

- **at very high Reynolds numbers**
- **with very small velocity sensors close to the wall**

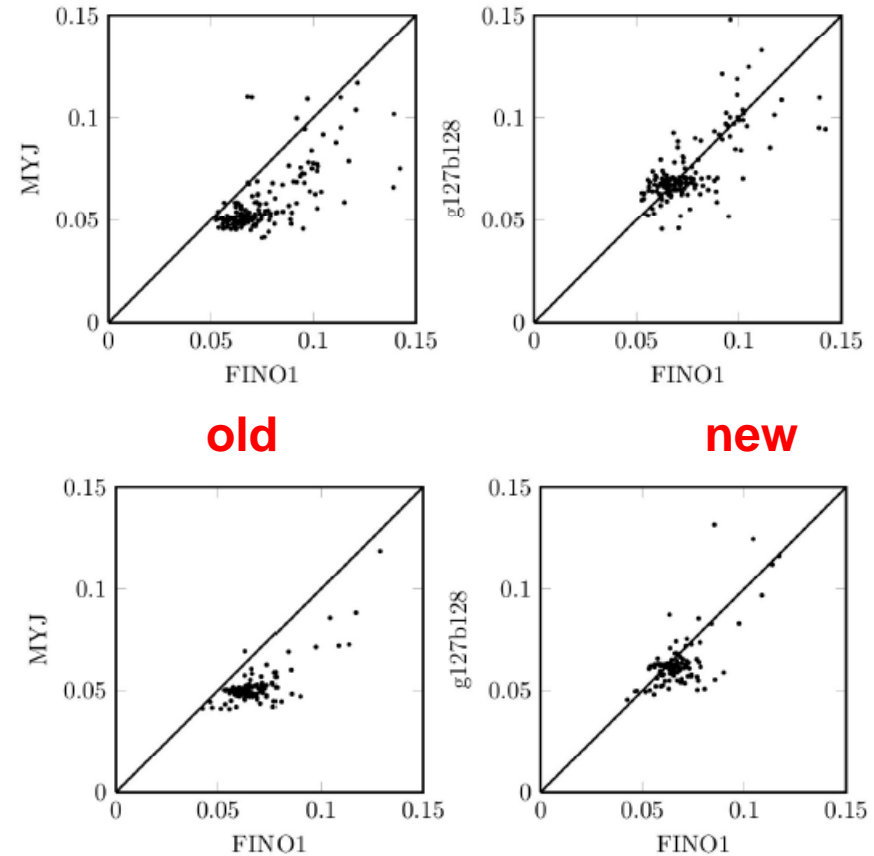
Foreman, R., S. Emeis, 2012: Method for increasing Turbulent Kinetic Energy in the Mellor-Yamada-Janjić boundary layer parametrization. accepted by Bound.-Lay. Meteorol.

comparison of model results with  
offshore (FINO1) and  
onshore (Caughey et al. 1979)  
data



vertical profiles of  
normalised turb. kin. energy  
January 2005

turbulence intensity at 80 m height  
February 2005



turbulence intensity at  
80 m height November 2005

# 2

## TUFFO idea

## TUFFO (August 1, 2011 to July 31, 2014)

Detection and assessment of the impact of **turbulent humidity (Feuchte) fluxes** on turbulence in **offshore** wind parks

### investigators:

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humid air is lighter than dry air

sea surface is a perfect humidity source

- near surface air is nearly saturated
- air aloft is less saturated

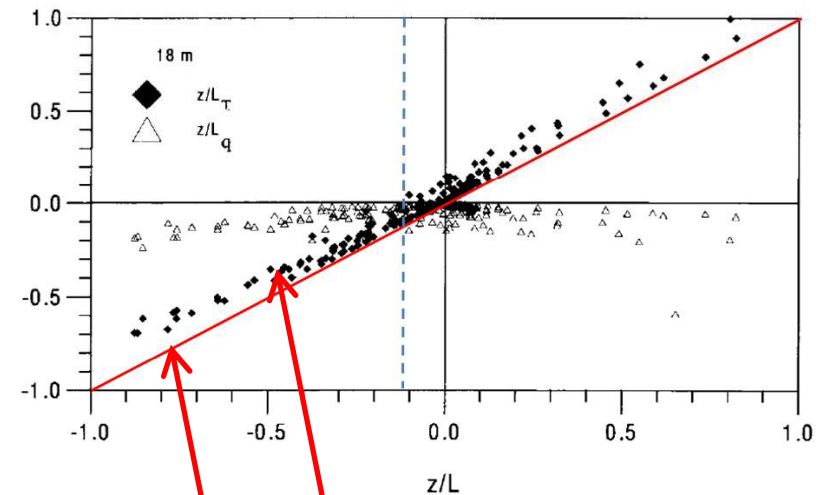
→ less static stability (in 30 to 50 % of all cases: humidity profile decides on static stability)

(Sempreviva and Gryning 1996, Edson et al. 2004)

→ more turbulence

→ more loads on turbines

→ less wake lengths behind turbines and wind parks



stability from  
temperature only  
true stability of air mass

## new approach in TUFFO:

**deployment of high-speed humidity sensors to FINO 1  
co-located with ultra-sonic anemometers**

- high-resolution humidity data
- turbulent vertical humidity fluxes
- better static stability information

**assessment of impact on turbulence at hub height**

**assessment of impact on wind parks (efficiency, wake lengths)**

**update of turbulence parameterization in meso-scale wind field  
models**

## Summary:

### VERITAS

#### sea surface drag description

**no wave data:** sea surface drag flattens off for high wind speeds

**with wave data:** sea surface drag depends on wave steepness squared

#### meso-scale wind field models

enhanced turbulence parameterization which gives higher (more realistic) turbulence intensities in the lower part of the atmospheric boundary layer

### TUFFO

#### vertical humidity structure in the marine boundary layer

leads to more unstable static stratification → more turbulence



Thank you very  
much for your  
attention

Gefördert auf Grund eines Beschlusses  
des Deutschen Bundestages



Bundesministerium  
für Umwelt, Naturschutz  
und Reaktorsicherheit

Projekträger

